# WASTEWATER ENGINEER’S REPORT 

Saratoga BioChar Solutions, LLC
Farnan Road
Town of Moreau, NY

March 30, 2022

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## PROJECT DESCRIPTON

The proposed Saratoga Biochar Solutions carbon fertilizer manufacturing facility utilizes biosolids and wood waste feedstock to produce a marketable carbon fertilizer through lower temperature drying and pyrolysis processes. Process and domestic wastewater generated by the facility will be connected to the existing Town of Moreau sewer collection system located in Moreau Industrial Park. Proposed infrastructure and connection include the installation of a 6 -inch diameter schedule 40 pvc pipe discharge line. This report summarizes the anticipated wastewater discharge volume, existing and proposed infrastructure required for the proposed development for consideration and review by the Town of Moreau.

## DESCRIPTION OF EXISTING SITE

The project site is comprised of two parcels located at the terminus of Farnan Road within the Moreau Industrial Park (MIP) in the Town of Moreau, NY (Tax Map IDs 50.-4-22 and 50.-4-16). The site is approximately 5.89 土acres of undeveloped land. The western portion of the site is currently wooded while the eastern extremities are primarily grassed with no existing development. Majority of the surrounding parcels are undeveloped with the exception of roads, a sanitary sewer pump station with perimeter fencing located at the southeast corner of the site, and a chemical manufacturing facility, Hexion, Inc., located across Farnan Road to the east of the project site.

The MIP is currently serviced by the Moreau sewer collection system via an 8-inch class 50 ductile iron sewer force main running along the east side of Farnan Road. A pump station (MIP pump station) exists on the west side of the cul-de-sac located at the terminus of Farnan Road. Per Laberge Group's Sewer District No. 1 Extension 5 Addendum 2 Report dated January 2021, the MIP pump station has a maximum 370 minutes per day operation with projected pumping at 2.75 minutes per cycle at 405 GPM . The current MIP activities are reported to be operating 30-40 minutes per day in the low to mid 300 GPM. The existing pump station has a 10 -foot diameter wet will with a reported 1.9-foot-deep active volume. The Laberge Group Report is provided in Appendix B of this report.

## DESCRIPTION OF PROPOSED DEVELOPMENT

Proposed site development includes the construction of a carbon fertilizer manufacturing facility (Facility), a parking lot and required stormwater management practices. The proposed Facility consists of a metal building constructed in three separate phases between 2022 and 2026. The Facility will manufacture a Class A carbon fertilizer from feedstock of primarily biosolids sourced from wastewater treatment plants. The manufacturing process implements drying and pyrolysis to produce the carbon fertilizer for use as soil fertilizer.

Proposed sewer infrastructure includes a 6-inch diameter schedule 40 pvc pipe. The discharge line will exit from the eastern most building and run through the eastern extremities of the site to an existing sanitary sewer manhole located on the west side of the Farnan Road cul-de-sac. The existing manhole currently has three inflow pipes and one outflow pipe that conveys wastewater to the MIP lift station.

## ANTICIPATED WASTEWATER PRODUCTION

The anticipated wastewater discharge generated by activities at the proposed Facility is 29,456 gallons per day (GPD) after the buildout of Phase 3. The breakdown of wastewater production at each phase is provided below and in Appendix A of this report. It is anticipated that two to six employees will be tending operations on a daily basis. The anticipated volume of wastewater estimation provided below. The Facility is anticipated to operate 24 hours, 7 days a week, with operational uptime estimated at $95 \%$ and downtime anticipated at $5 \%$ for scheduled maintenance. As such, discharge of wastewater is assumed to be relatively continuous.

| Anticipated Wastewater Flow Rates |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Phase 1 | Phase 2 | Phase 3 | Total |  |
| Hourly Demand <br> (GPH) | 422 | 402 | 402 | 1,227 |  |
| Daily Demand <br> (GPD) | 10,139 | 9,659 | 9,659 | 29,456 |  |

Note: See Appendix A for breakdown of wastewater production within the proposed process line following the buildout of each phase.

## AVAILABLE SEWER COLLECTION CAPACITY

The Town of Moreau sewer collection system currently has five sewer district extensions that ultimately discharge to the City of Glens Falls Wastewater Treatment Plant (WWTP). Wastewater must meet the Glens Falls City Code 177 Article VII Discharge Requirements prior to discharge to the municipal sewer system. As provided in letter composed by the chief operator of the City of Glens Falls WWTP, the Town of Moreau's discharge capacity is currently 190,000 GPD while reported discharge is presently 75,000 GPD. As such, remaining capacity is adequate to accommodate collection and treatment of wastewater discharge from the Saratoga Biochar Solutions Facility.

The existing MIP pump station has the capacity to run at 405 GPM at 2.75 minutes per cycle. The anticipated wastewater discharge rate after Phase 3 buildout is 21.4 GPM, far below the maximum pump capacity reported in the Laberge Group Report (Appendix B).

## CONCLUSION

It is our opinion that the existing MIP sewer collection system infrastructure is capable of accommodating the connection and conveyance of wastewater generated by proposed development. Additionally, based on discharge capacity provided by the City of Glens Falls WWTP chief operator, the WWTP has adequate capacity to accommodate to manage the additional discharge produced by proposed development.

Water Engineer's Report Prepared by:


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Principal
For
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> APPENDIX A
> SARATOGA BIOCHAR ESTIMATED WASTEWATER PRODUCTION

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## Providing Essential Services - Manufacturing Carbon Fertilizer - Benefiting Host Communities \& Environment

## SBS Water \& Wastewater Requirements

Note: SBS intends to recycle the wastewater from the ammonia scrubber into the carbon fertilizer to avoid nutrient discharge to the sewer. The wastewater replaces water that would otherwise be consumed from the municipality to hydrate the carbon fertilizer.

| SBS Water |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | :---: | :---: | :---: | :---: | :---: |
|  | Phase 1 | Phase 2 | Phase 3 | Total | Units |  |  |  |  |  |
| Process | $\mathbf{3 6 8}$ | $\mathbf{3 6 8}$ | $\mathbf{3 6 8}$ | $\mathbf{1 , 1 0 3}$ | GPH |  |  |  |  |  |
| Venturi Scrubber | 259 | 259 | 259 | $\mathbf{7 7 8}$ | GPH |  |  |  |  |  |
| Sulfur Dioxide (SO2) Scrubber | 74 | 74 | 74 | $\mathbf{2 2 3}$ | GPH |  |  |  |  |  |
| Ammonia (NH4) Scrubber | 13 | 13 | 13 | $\mathbf{3 9}$ | GPH |  |  |  |  |  |
| Bioscrubber | 21 | 21 | 21 | $\mathbf{6 3}$ | GPH |  |  |  |  |  |
| Office |  |  |  |  |  |  |  |  |  |  |
| Truck Wash | 30 | 5 | 5 | 40 | GPH |  |  |  |  |  |
|  | 60 | 25 | 25 | 110 | GPH |  |  |  |  |  |
| Total, hourly |  |  |  |  |  |  |  |  |  |  |
| Total, daily | $\mathbf{4 5 8}$ | $\mathbf{3 9 8}$ | $\mathbf{3 9 8}$ | $\mathbf{1 , 2 5 3}$ | GPH |  |  |  |  |  |
|  | $\mathbf{1 0 , 9 8 6}$ | $\mathbf{9 , 5 4 6}$ | $\mathbf{9 , 5 4 6}$ | $\mathbf{3 0 , 0 7 9}$ | GPD |  |  |  |  |  |


| SBS Wastewater |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Phase 1 | Phase 2 | Phase 3 | Total | Units |
| Process | 391 | 391 | 391 | 1,174 | GPH |
| Venturi Scrubber |  |  |  |  |  |
| Discharge | 259 | 259 | 259 | 778 | GPH |
| Dust (biosolids) | 2.2 | 2.2 | 2.2 | 6.7 | $\mathrm{lbs} / \mathrm{h}$ |
| Sulfur Dioxide (SO2) Scrubber |  |  |  |  |  |
| Discharge | 92 | 92 | 92 | 276 | GPH |
| Calcium Sulfite $\mathrm{CaSO} 3 \times \mathrm{x}$ ( H 2 O ) | 147 | 147 | 147 | 440 | $\mathrm{lbs} / \mathrm{h}$ |
| Ammonia (NH4) Scrubber |  |  |  |  |  |
| Discharge | 19 | 19 | 19 | 57 | GPH |
| Ammonium Sulfate $\left(\mathrm{NH}_{4}\right)_{2} \mathrm{SO}_{4}$ | 49 | 49 | 49 | 146 | $\mathrm{lbs} / \mathrm{h}$ |
| Bioscrubber |  |  |  |  |  |
| Discharge | 21 | 21 | 21 | 64 | GPH |
| Office | 25 | 5 | 5 | 35 | GPH |
| Truck Wash | 25 | 25 | 25 | 75 | GPH |
| Total, hourly | 441 | 421 | 421 | 1,284 | GPH |
| Total, daily | 10,593 | 10,113 | 10,113 | 30,819 | GPD |
| Total, minus NH4 Scrubber, hourly | 422 | 402 | 402 | 1,227 | GPH |
| Total, minus NH4 Scrubber, daily | 10,139 | 9,659 | 9,659 | 29,456 | GPD |

APPENDIX B<br>LABERGE GROUP<br>SEWER DISTRICT NO. 1 EXTENSION 5<br>ADDENDUM 2<br>REPORT

Town of Moreau
Saratoga County, New York
Map Plan and Report
Sewer District No. 1 Extension 5

## ADDENDUM 2

January 2021


## PREPARED FOR:

Town of Moreau
351 Reynolds Road
Moreau, New York 12828

## PREPARED BY:



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# Town of Moreau <br> Saratoga County, New York <br> Map Plan and Report <br> Sewer District No. 1 Extension 5 

## ADDENDUM 2

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Attachment C: Hydraulic Grade Line Maps
Attachment D: Lift Station Design Basis
Attachment E: Buoyancy Calculations
Attachment F: System Schematic
Attachment G: Sewer System Readings

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## INTRODUCTION

This report is intended to supplement the previously submitted "Map, Plan and Report / Sewer District No. 1 / Extension 5" dated May 2018 and Report Addendum 1 dated November 2019, prepared by Laberge Group. This report provides the specific technical design information relating to the plans and specifications for the Town of Moreau's Sewer District No. 1, Extension No. 5 (the "Extension").

## I. GENERAL

The project includes the installation of a low pressure sewer collection system and associated grinder pumps, central lift station and forcemain.

## II. COLLECTION SYSTEM

The collection system will be of the low pressure type.
The E-One design report contained in Attachment A presents sizing information for of the low-pressure sewer. There are four generalized areas that contribute flow to the extension's central lift station:
A. West of the central Lift Station on Route 9:37 grinder pump stations flow through pipe varying from 2 -inch to 4 -inch diameter.
B. East of the central Lift Station on Route 9: 16 grinder pump stations discharge through a pipe varying from 2 -inch to 4 -inch diameter.
C. Pines Trailer Park: 16 grinder pump stations with discharge through a pipe varying from 2 -inch to a 3-inch diameter.
D. Lamplighter: 115 grinder pump stations and an additional 53 pumps on Route 9 discharge through pipe varying from 2 -inch to 4 -inch diameter.

The Central Lift Station discharges through a ten-inch HDPE force main that is discussed later in the report.
In addition to the above-noted grinder pumps, there are 11 grinder pumps to be installed at the Bluebird Terrace mobile home park. A small low pressure sewer collection system in this park is comprised of 2-inch diameter pipe. This low-pressure sewer system will extend toward the ten-inch force main at its alignment station $239+35$, but it will not connect to that force main. Rather, the two-inch low-pressure sewer will be installed along-side the ten-inch line up to alignment station $274+10 \pm$, approximately 3,475 linear feet, to a point where it will connect to the 6 -inch force main from Bluebird Village (not from the Central Lift Station) that runs parallel to the Central Lift Station's force main. The 6 -inch force main connects to the Industrial Park force main, which discharges to the City of Glens Falls.

This approach is pursued for two reasons: first, the owner can pursue a separate funding opportunity for a separated new low-pressure sewer. Second, this presents an opportunity to connect Bluebird Terrace to the Glens Falls WWTP, sooner than other project components.

## Low-Pressure Sewer System Design

Wherever possible, multiple dwellings on individual lots will be combined into common grinder pump stations. In the case of mobile homes, three or four residences will typically share a grinder pump, but no more than six residences per grinder pump station will be allowed. Businesses will each have their own grinder pump(s). In the case of where a single grinder pump station serves a single dwelling or mobile home, a simplex grinder pump station will be installed which provides 100 -gallons of storage volume. In cases where a single grinder pump station serves multiple residences, a duplex grinder pump station will be provided with up to 476-gallons of storage volume.

For lodging establishments, there was an assessment of water meter data and existing septic tank capacity to tailor the grinder pump storage capacities to these individual businesses. As such, establishments will be provided one or more fiberglass tanks with volumes ranging from 630 gallons to 1,700 gallons. Basic sizing was specified based on the following:

- No less than 70 gallons storage will be provided for each equivalent dwelling unit.
- Commercial basin sizing used available drinking water meter data to establish equivalency based on 200 gallons per day (GPD) estimated dwelling usage.
- Where existing pump or holding tanks are in use, these tanks will be replaced with new matching sized tanks with formed inverts to convey flows to the pumps.
- Grinder pump control boxes will be supplied with power outlets capable of being energized by a portable generator during a prolonged power outage.

The proposed grinder pumps will have sufficient head capacity to meet the demand for this system. As demonstrated by the pump curve for the grinder pump units contained in Attachment $\mathbf{B}$ the pumps have a head capacity of 185 feet, more than sufficient for this application.

The low pressure sewers will contain flushing access at the terminal ends and on line depending upon length. Air release valves are located high points throughout the system.

## III. FORCE MAIN

The central Lift Station is to be installed near station $64+50 \pm$ on Route 9 with a 10 -inch HDPE SDR 11 force main connecting to the existing 8 -inch DIP Industrial Park force main in Sisson Road at approximately station $298+80 \pm$. There is a total of $23,580 \pm$ feet of proposed 10 -inch HDPE. The proposed 10 -inch diameter HDPE force main is rated for 200 psi . Please refer to Attachment C for the force main hydraulic grade line.

The existing Industrial Park force main discharges to the existing Manhole 5 at the Glens Falls Waste Water Treatment Plant. The existing force main is generally lower in elevation than the proposed main, with a high point of 320 feet at an air valve that is upstream of where the profile sags significantly to cross the Hudson River. The overall length of new and existing force main is $35,510 \pm$ feet.

The end-to-end elevation change on the overall force main is from $334 \pm$ feet at the lift station to $297 \pm$ feet at Manhole 5, with the highest elevation being $344 \pm$ feet near stations $144+80$ and $243+20$ feet.

The proposed 10 -inch force main shall be provided with air release valve structures at high points averaging about 3200 feet apart. These valves serve primarily to release air during force main pressurization, as vacuum pressure is less of a concern with the small pipe diameter, low pressures, and small elevation changes. The design basis for the air release valve is the Valmatic 48A for 150 psi cold pressure with a $3 / 16$-inch orifice. Special attention is afforded to the air valves at STA $242+90 \pm$, which are at the top and bottom of a 25 -foot net drop; there, the design basis is the Valmatic 801A single-body combination air valve with a 1 -inch large outlet and a $1 / 8$-inch small orifice. Each valve will have a ball valve in between the force main and the valve for the valve's isolation during maintenance or replacement. The new force main shall also be provided with flushing stations at no more than 1,000 -foot intervals.

## IV. CENTRAL LIFT STATION

## A. General Description

This central Lift Station will be of the submersible duplex type. The pump operation will be controlled by a level transducer, with operating levels to trigger the low level pump off, lead pump on, lag pump on, and high water alarm. A redundant pump level control system using float switches is also incorporated into the design. The station will be fitted with a flushing valve or similar mechanisms to agitate the wet well sump to dislodge settled materials before discharge.

The station will also include:

- Wet well

The wet well is to be a 10 -foot diameter concrete structure. Sizing information is presented in Section $G$ below.

- Inlet manhole

The four-inch LPS pipeline terminates at the inlet manhole that will drain to the wet well through a 18 -inch gravity sewer. There is a 6 -inch stub also connected to this manhole for future expansion if required.

- Valve / metering vault

The valve vault combines the pump discharges where they are connected to the force main and by-pass connection. Check valves and air release valve are provided on both discharge lines from the pumps and a magnetic flow meter is to be installed on the force main prior to exiting the vault. The vault will have a seven-foot interior ceiling height and be set belowgrade with lighting, hatch access, retractable ladder, and sump pump for any seepage or released wastewater that may escape during any maintenance or repair. The sump pump discharges back into the wet well.

- Control building

The control building will contain the electrical panels for pump control, main service, SCADA, automatic transfer switch, and appurtenant items. It will be heated, ventilated, and have interior lighting.

- Emergency Standby Generator

The site shall have a stationary generator that is fueled by natural gas. The design basis is a Cummins RS80 3-phase 80 kW generator set. The generator is protected behind bollards and fencing, and is set on an equipment pad that provides at least four feet clear for maintenance access.

- Miscellaneous Site Improvements including:
- Fencing with a remotely-operated sliding gate and pedestrian pass gate.
- Site lighting
- Access drive and parking area
- Landscaping
- Stormwater detention and infiltration
- Yard hydrant for wash water


## B. Flow Estimates

Two methods were employed to estimate the flow to the lift station: an empirical analysis prepared by E-One and a typical water use analysis.

## 1. Empirical Analysis

E-One has an empirical design analysis method, which uses the maximum discharge rate for a pump and applies a factor for how many pumps are expected to operate simultaneously which in turn identifies the peak flow anticipated at the lift station. Based on that analysis, areas A thru D identified in Section II Collection System are expected to have a maximum of nineteen (19) simultaneously operating pumps to produce as much as two hundred nine (209) gallons per minute (GPM). The E-One report is in Attachment A.
2. Water Use Analysis

The water use analyzed in the Map, Plan and Report prepared by Laberge Group and dated May 2018, and Report Addendum 1 dated November 2019, used water meter data of the properties in the sewer district. The existing average daily flow is 55,000 GPD. The additional flow from build out of vacant parcels was estimated at 54,000 GPD for a projected average daily flow of 109,000 GPD or approximately 75 GPM. Using a peaking factor of four (4.0) results in a peak hour flow rate of 300 GPM.

## C. Minimum Flow Rate

The ten-inch HDPE pipe has an average inside diameter of 8.68 inches. The existing Industrial Park 8 -inch class 50 ductile iron pipe to which the HDPE pipe connects has an inside diameter of 8.5 inches. The 10 -inch HDPE was selected to best fit the ductile iron pipe diameter.

The flow required to achieve a minimum velocity (V) of 2.0 feet per second, assuming that only the Extension lift station is operating is:

$$
\mathrm{Q}_{\min }=\mathrm{VA}=\mathrm{V} \pi \mathrm{D}^{2} / 4=(2.0 \mathrm{ft} / \mathrm{s})(\pi)(8.68 \mathrm{in})^{2}(8.68 / 12) / 4=0.82 \mathrm{ft}^{3} / \mathrm{s}=\mathbf{3 6 9} \mathbf{~ G P M}
$$

## D. Total Dynamic Head

1. Elevation Head

- Pump elevation (pump-off) $=331.4$ feet
- Discharge elevation $=256$ feet (Glens Falls MH 5)
- Highest Points $=344$ feet, at Stations $144+80 \pm$ and $243+20 \pm$
- Design High Point $=320$ feet, at STA 366+60 (on the existing main)

Elevation Head to Discharge $\quad=(75.4) \mathrm{ft}$
Elevation Head to Highest Point $=12.6 \mathrm{ft}$
Elevation Head to Design High Point $\quad=(11.4) \mathrm{ft}$
2. Minor Losses (Equivalent Length)

Extension HDPE force main:

| Fitting | Count | LF/ea | Sum |
| :--- | :--- | :--- | ---: |
| - Gate valves (at flush valves, etc.) | 54 | 4.5 | 243 ft |
| - 90-degree bends (at the station) | 2 | 20.0 | 40 ft |
| - 45-degree bends | 8 | 10.0 | 80 ft |
| - Tee wye (as std. tee) | 1 | 14.0 | 14 ft |
| - Swing check valve | $\underline{1}$ | 50.0 | 50 ft |
|  | Minor losses | 427 ft |  |
|  | Measured pipe length | $23,580 \mathrm{ft}$ |  |
|  | Equivalent length | $24,007 \mathrm{ft}$ |  |

Existing DIP force main (counts are from Stearns \& Wheeler's pipe layout plans, 1996):

| Fitting | Count | LF/ea | Sum |
| :---: | :--- | :--- | ---: |
| - 90-degree bends | 1 | 20.0 | 20 ft |
| - 45-degree bends | 4 | 10.0 | 40 ft |
|  | Minor losses | 60 ft |  |
|  | Measured pipe length | $6,780 \mathrm{ft}$ |  |
|  | Equivalent length | $6,840 \mathrm{ft}$ |  |

3. Friction Losses

Pipe friction losses are calculated using the equation.

$$
\mathrm{V}=1.318 \mathrm{CR}^{0.63} \mathrm{Hf}^{0.54}
$$

|  | HDPE Pipe Section | DIP Pipe Section |
| :---: | :---: | :---: |
| Flow Rate (Q) | 567 GPM (1.3cfs) | 567 GPM (1.3cfs) |
| C-Value | 120110 |  |
| Inside diameter | 8.68 inches ( 0.72 ft ) | 8.50 inches ( 0.71 ft ) |
| Area (A) | 0.41 sf | 0.39 sf |
| Hydraulic Radius (R) | 0.181 ft | 0.177 ft |
| Velocity (V=Q/A) | 3.07 fps | 3.20 fps |
| Friction Loss ( $\mathrm{H}_{\mathrm{f}}$ )/ft | $0.0050 \mathrm{ft} / \mathrm{ft}$ | $0.0064 \mathrm{ft} / \mathrm{ft}$ |
| Equivalent Length | 24,007 feet | 6,360 feet |
| Friction Loss | 118 feet | 41 feet |

Total Friction Loss $=118$ feet $+\mathbf{4 1}$ feet $=159$ feet
E. Computed Total Dynamic Head

The total dynamic head on the pump has been calculated using the design high point in the existing 8 -inch DIP force main located just before the drop down the hill to the Hudson River. This point was selected since using the actual discharge elevation at Manhole 5 would induce a significant negative elevation head resulting in the main at the above referenced high point experiencing a negative pressure. To eliminate the negative pressure, the elevation head has been adjusted based on the design high point elevation and is reduced to negative 14 feet rather than negative 78 feet. The existing force main has an air valve at the design high point.

Total Dynamic Head, Design High Point
Elevation Head= (11)
Friction/minor losses
HDPE $=24,007$ lf $x 0.0050=118$
$\underline{\mathrm{DIP}}=6,840$ lf $\mathrm{x} 0.0064=41$
TDH $=148$

## F. Pump Selection

The pump selected for this application is the Xylem's Flygt NP3171 SH3 275, 35 HP, or the Landustrie DWP62-41LI, 52HP, or equal. See Attachment D for relevant pump curves.

## G. Wet Well

Average Flow Rate $\quad=\quad 75 \mathrm{gpm}$
Fill time $=20$ minutes
Volume required $=75 \mathrm{gpm} \times 20 \mathrm{~min} . \quad=1,500$ gallons.
1,500 gallons ( 200.5 cubic feet) of active storage is to be provided by a ten-foot diameter wet well as calculated with the following equation:
$\mathrm{V}=\pi \mathrm{D}^{2} \mathrm{~h} / 4$
$200.5 \mathrm{cf}=\pi\left(10 \mathrm{ft}^{2}\right) \mathrm{h} / 4$
$\mathrm{H}=2.55$ feet; USE 2.6 feet
Wet Well Elevations:

- Inlet invert Elevation 337.5
- High water alarm 335.5
- Lag pump on 334.5
- Lead pump on 334.0
- Pump off 331.4
- Low level alarm 331.0
- Floor elevation 329.4


## H. Buoyancy

Both the wet well and valve vault were checked for buoyancy, with both structures being designed to resist buoyancy. Calculations for buoyancy are included in Attachment E. Please note however that boring results along the corridor found well drained sand and no groundwater at proposed improvements.

## V. DOWNSTREAM CONSIDERATIONS

## A. Down Stream Facilities

There are five privately owned and one municipal downstream pump stations that are potentially influenced by this Extension. A schematic diagram of the station locations and pumping characteristics is included as Attachment F. These stations include:

- Moreau Industrial Park (MIP)
- Bluebird Village Apartments
- Home of the Good Shepard
- Sisson Reserve Apartments
- Harrison Quarry / Bluebird Trace Apartments
- Harrison Place Apartments

In addition, there are four additional future developments seeking to connect to the existing 8 -inch DIP forcemain. These include:

- Leonelli Apartments on Harrison Ave. (construction is in progress)
- Bluebird Trace Apartments (construction is in progress)
- Va-va-Voom mixed use development
- Sisson Grove Apartments

There are several restrictions on pumping operations at the privately owned pump stations, based upon the various design reports. The private pump stations receive communications from the MIP via licensed radio transmissions for a "passive interlock".

- Leonelli Apartments and Sisson Reserve pump station operations were initially restricted when the MIP station was operating. A subsequent design report indicated that Sisson Reserve would allow operation when the MIP station was operating in the event of a high water alarm. A revised Leonelli Apartments' design report (dated October 2020) indicated no operation when the MIP station was operating.
- Bluebird Village operation was to be restricted when any of MIP, Sisson Reserve, or Leonelli Apartments were operating.
- Harrison Quarry / Bluebird Trace operation was to be restricted when the MIP was operating.
- Harrison Place has no restrictions listed in the design report, but agreements with the Town require pumping to occur only when the MIP is idle.


## B. Overview of Downstream Pump Stations

- Moreau Industrial Park (MIP)

Development: A partially developed industrial park.
Pump: In the report for the Harrison Avenue projects, the MIP pump station is reported to have a 370 minutes per day operation at maximum buildout, with a then projected pump operation of 30-40 minutes per day, citing Industrial Park pumping at 2.75 minutes per cycle at 405 GPM . Current industrial activity causes the pump to operate at less than 30 minutes per day and is reported by the Town to operate in the low-to-mid 300 GPM. Pump cycle timing will vary widely, depending upon the industrial operations.

The station has a 10 -feet diameter wet well with the record drawing noting a 1.9 foot deep active volume. The Town reports having aggregate run time data but no cycle data. The pump is reportedly an ABS AFP (K) 1047.1 ME 185/4. 0018507, 24.8 hp , 460 v , 3phase. There is no immediately available data for the pump with the town, online, or with the pump manufacturer. This is a long discontinued pump, showing its age, and the Town has discussed pump replacement.

## - Leonelli's Apartments on Harrison Avenue (Ext. No. 1)

Development: This project has two parts; the first part with 240 units of the Harrison Avenue project are still to be constructed, while the second part was replaced by the Sisson Reserve project and is now constructed. The latest informal design information lists a 36,000 GPD average flow with a 100 GPM peak hour flow.

Piping: A 6-inch diameter, 1,300 $\mathrm{lf} \pm$ force main with an elevation gain of approximately 12 feet connects to the MIP force main.

Pump and wet well: The pump station wet well was reportedly 9'-6" diameter with a 3.45 -foot active volume ( 1829 gallons). With the restart of the project and a new design report, the wet well will have 745 gallons and a Landustrie DWP22-40DG pump. The minimum flow rate will be 180 GPM @ 20-23 feet TDH and the operating point will be 255 GPM at 30.8 feet TDH. Approval of the design report or pump station plans have not been granted by the Town and formal review is pending. For a conservative approach, this report assumes the system shown in the design report will be constructed even though additional wet well capacity will likely be required.

- Sisson Reserve (Replaced Leonelli's Sisson Road)

Development: This development proposed 145 units and a $10 \%$ future expansion factor.
Piping: The design report lists a four-inch diameter 1,127 if of force main that connects to the MIP force main, with no indication of pipe materials.

Pump: Pump performance is unclear in the report text, listing a $98-\mathrm{ft}$ Total Dynamic Head and 133 GPM inflow to the existing pump station. The appendices list a 136 GPM peak hour inflow, a $6^{\prime}-0$ " diameter wet well, and a pump start analysis using a 423 -gallon wet well with 19 starts per hour. Four sets of curves are provided at the end of the report. It appears that the 98 ft TDH in the report refers to a combined flow with the MIP and is indicated to occur upon a high alarm condition at 155 GPM, and the Sisson Reserve flow alone would then be 250 GPM at 95 feet TDH.

- Bluebird Village (Ext. No. 2)

Development: The development is comprised of 244 two and three bedroom apartments.
Piping: The pipe system is reported to be 2,500 feet of six-inch diameter pipe. It is assumed that this is a PVC pipe with $\mathrm{C}=120$.

Pump: The design report for this extension indicates a peak hour inflow of 82 GPM and a design discharge of 180 GPM for a 10 -minute pumping cycle ( 200 GPM at 27 feet TDH, per the drawings). Record drawings indicate an 8 -foot diameter wet well with a 2.2 foot depth from pump off to pump on, for a storage volume of 400 gallons. Per some record drawings, the pumps are Gorman-Rupp T3A-B. Building

Department records indicate a T3A-B-4 curve on a 7.5 HP T3A-B pump was originally used for the project; our office has been informed the pumps were changed out to Landustrie DWP42-43FE with 925 mm impellers, which provide a maximum head of 31.5 feet. The Town reports that no high water alarms are reported with these new pumps over several months.

Coordinated Operation: By agreement this system was to be designed so that it operates only when other systems are not operating, with the other systems at that time (Leonelli projects on Harrison Avenue and Sisson Road and the industrial park) stated to be collectively pumping 490 minutes per day and 3 minutes per cycle at each station.

- Harrison Place

Development: Twenty-six apartment units.
Pipe: There is a two-inch force main that combines flow from the two grinder pump stations.

Pumps: This system employs four grinder pumps split between two pump stations, and with an assertion that the cumulative flow is 9 GPM. Using the previously mentioned empirical model, three of the four pumps may operate simultaneously and inject approximately 33 GPM into the force main at potentially high head, so there should be no difficulty in overcoming flows in the current proposal. The 33 GPM is used for peak hour analyses.

- Harrison Quarry / Bluebird Trace

Development: This development was proposed to contain 186 units.
Pipe: The design report states that there is 2,300 linear feet of 6 -inch pipe. For analysis, the pipe is assumed to be $\mathrm{PVC}, \mathrm{C}=120$.

Pump: The design report lists an estimated peak hour flow of 68 GPM into a wet well that has a design discharge of 230 GPM. Data obtained from Smith \& Loveless indicates each pump (Model 4B2D) was to have a design point of 230 GPM at 69 feet TDH.

- Home of the Good Shepard (a.k.a. Nest Phase 1)

This development does not appear to have a design report, and is listed by Environmental Design Partnership as contributing 12 GPM to the system.

- The aggregate flow from the above pump stations is metered prior to discharge to the City of Glens Falls. The meter became operational in March of 2020. The aggregate discharge falls in the range of 2.2 MG to 2.4 MG in a month, which translates to an average daily flow of 73,300 to 80,000 GPD.


## C. Coordination and Performance of the larger system

An analysis of the Extension lift station operating against other individual pump stations was performed, with pump operation frequencies in the range of 40 hz to 50 hz . Operating at 60 hz would further impede other pumps' discharge rates.

The table below presents the Extension lift station operating against each of the downstream pump stations including the resultant flow rate from each station, the TDH on each pump, velocity in the discharge main from each station and the pump run time to draw down the wet well.

| Scenario | FLOW <br> (GPM) | TDH <br> (FT) | VEL. <br> (FPS) | PK. HR. PUMPING <br> (MIN.) |
| :--- | :--- | :--- | :--- | :--- |
| Extension | 567 | 144 | 3.2 | 5.3 |
| Extension (50 hz) | 454 | 104 | 2.6 | 8.5 |
| Leonelli Apts. | 250 | 31 | 2.8 | 5.7 |
| Extension (50 hz) | 447 | 106 | 2.4 | 10.3 |
| Harrison Quarry | 210 | 75 | 2.4 | (Note 1) |
| Extension (50 hz) | 440 | 107 | 2.5 | 12.2 |
| Sisson Reserve | 215 | 97 | 5.5 | 3.6 |
|  |  |  |  |  |
| Extension (45 hz) | 567 | 144 | 3.1 | 5.6 |
| Bluebird Village | - | 31.5 | - | (Note 2) |
| Extension (at 45 hz) | 355 | 92 | 1.9 | (Note 3) |
| MIP | 315 | 164 | 1.8 | - |

(1) The wet well size is not identified in the Design Report for Harrison Quarry / Bluebird Trace
(2) Bluebird Village appears to be unable to pump against the head imposed by the Extension's pump and will need to be restricted from operation when the MIP or extension are pumping at full capacity.
(3) The operation of the Extension against the MIP noted above, with 1.9 FPS flow, is a transitory condition; when the MIP stops pumping, the Extension's pump will increase its flow rate to above 2 FPS flow.

## D. Proposed Operation

1. The MIP and the Extension stations can operate at any time and will use the MIP's interlock signal to stop or hold operation of the other pump stations.
2. The Extension's pump will operate at a lower frequency of $45 \pm$ hertz to allow the MIP's operation. If the MIP is not operating, then the Extension's pump will operate at 60 hertz.

If future development increases flows into the Extension, then the extension will simply pump more frequently, or the "pump on" level could also be raised to provide additional storage volume.

If there is an upgrade to the MIP, then the $45 \pm \%$ hertz frequency cap can be increased, to optimize the flow and to reduce overall cycle time.

Furthermore, if there is substantial development, then the proposed force main could be later extended along a path parallel to the existing force main. This project includes a dead-end force main stub past the connection to the existing force main, in order to allow such an extension while maintaining operation. Such a force main extension would provide either selective isolation of stations or additional peak hour capacity to optimize overall system capacity.

## E. Communication

In the near term, to transmit signals and data between the Extension and the MIP, it is proposed to install radio transmission/reception equipment that is compatible with the MIP's existing control equipment and modify the existing signal algorithm.

## F. Operations and Maintenance

The proposed system will be operated and maintained by the Town of Moreau Water and Sewer Department.

## ATTACHMENT

A

E-ONE DESIGN REPORT

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## Environment One Corporation

# Pressure Sewer Preliminary <br> Cost and Design Analysis 

For

## Moreau, NY

 rev. 2 opt. 1Prepared For:
Laberge Group
4 Computer Drive West
Albany
NY 12205
US
Tel: (518) 458-7112 x171
Fax:
Prepared By: N. Shafarzek

# Moreau, NY <br> rev. 2 opt. 1 

Prepared by:N. Shafarzek
On: April 29, 2020

## Notes :

Station recommendations preliminary. Analysis based on drawings and data provided.
GPD values effect retention times only, not line sizing or hydraulics.
DH151-93 standard in this analysis unles otherwise noted.
rev. 1 - added $\sim 33$ stations to main rd. per Laberge Group. Advise that you add new line for western sewer extension if looking to maintain scouring velocity. Eastern Sewer Extension (possible 15 add'l pumps) may be workable with proposed 2"-3" (zones 7-9) depending on how far the stations are from this system.
rev. 2 - updated layout per Christopher Wren. added lift station.
opt. 1-lift station to the south of lamplighter acres. additional stations cannot be accommodated with this lift station location without compromising design prior to buildout.

## Budgetary Low Pressure Sewer System Costs

Moreau, NY
rev. 2 opt. 1


Note: The System Costs above are based on piping sized for, and Grinder Pumps manufactured by Environment One Corporation.


| $\begin{gathered} \text { Zone } \\ \text { Number } \end{gathered}$ | Connects to Zone | Number of Pumps in Zone | Accum Pumps in Zone | Gals/day per Pump | Max Flow Per Pump (gpm) | $\begin{array}{\|c\|} \hline \text { Max } \\ \text { Sim Ops } \end{array}$ | $\begin{array}{\|l\|} \hline \text { Max Flow } \\ \text { (GPM) } \end{array}$ | Pipe Size (inches) | Max <br> Velocity (FPS) | Length of Main this Zone | Friction Loss <br> Factor <br> (ft/100 ft) | Friction Loss This Zone | $\begin{aligned} & \text { Accum Fric } \\ & \text { Loss (feet) } \end{aligned}$ | Max Main Elevation | Minimum Pump Elevation | Static Head (feet) | Total <br> Dynamic <br> Head (ft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| This spread | sheet was | lculated | sing pip | e diameters | for: SDR | 11HDPE |  |  |  | Friction loss calculations were based on a Constant for inside roughness "C" of: 150 |  |  |  |  |  |  |  |
| 36.00 | 37.00 | 10 | 28 | 120 | 11.00 | 5 | 55.00 | 3.00 | 2.74 | 408.00 | 0.98 | 4.01 | 35.27 | 355.00 | 351.00 | 4.00 | 39.27 |
| 37.00 | 42.00 | 0 | 90 | 120 | 11.00 | 8 | 88.00 | 4.00 | 2.65 | 53.00 | 0.69 | 0.37 | 31.26 | 355.00 | 351.00 | 4.00 | 35.26 |
| 38.00 | 39.00 | 9 | 9 | 120 | 11.00 | 3 | 33.00 | 2.00 | 3.57 | 242.00 | 2.52 | 6.10 | 51.36 | 355.00 | 350.00 | 5.00 | 56.36 |
| 39.00 | 40.00 | 9 | 18 | 120 | 11.00 | 4 | 44.00 | 3.00 | 2.19 | 301.00 | 0.65 | 1.96 | 45.26 | 355.00 | 347.00 | 8.00 | 53.26 |
| 40.00 | 41.00 | 12 | 30 | 120 | 11.00 | 5 | 55.00 | 3.00 | 2.74 | 430.00 | 0.98 | 4.22 | 43.30 | 355.00 | 348.00 | 7.00 | 50.30 |
| 41.00 | 42.00 | 14 | 44 | 120 | 11.00 | 6 | 66.00 | 3.00 | 3.29 | 595.00 | 1.38 | 8.19 | 39.08 | 355.00 | 349.00 | 6.00 | 45.08 |
| 42.00 | 43.00 | 0 | 134 | 120 | 11.00 | 9 | 99.00 | 4.00 | 2.98 | 100.00 | 0.86 | 0.86 | 30.89 | 355.00 | 349.00 | 6.00 | 36.89 |
| 43.00 | 44.00 | 4 | 164 | 120 | 11.00 | 10 | 110.00 | 4.00 | 3.31 | 243.00 | 1.04 | 2.54 | 30.03 | 355.00 | 350.00 | 5.00 | 35.03 |
| 44.00 | 64.00 | 11 | 175 | 120 | 11.00 | 10 | 110.00 | 4.00 | 3.31 | 1,305.00 | 1.04 | 13.63 | 27.49 | 355.00 | 350.00 | 5.00 | 32.49 |
| 45.00 | 64.00 | 4 | 4 | 120 | 11.00 | 3 | 33.00 | 2.00 | 3.57 | 112.00 | 2.52 | 2.82 | 16.68 | 355.00 | 350.00 | 5.00 | 21.68 |
| 46.00 | 47.00 | 3 | 3 | 120 | 11.00 | 2 | 22.00 | 2.00 | 2.38 | 102.00 | 1.19 | 1.21 | 43.20 | 356.00 | 352.00 | 4.00 | 47.20 |
| 47.00 | 48.00 | 6 | 9 | 120 | 11.00 | 3 | 33.00 | 2.00 | 3.57 | 431.00 | 2.52 | 10.86 | 41.99 | 356.00 | 350.00 | 6.00 | 47.99 |
| 48.00 | 49.00 | 9 | 18 | 120 | 11.00 | 4 | 44.00 | 3.00 | 2.19 | 266.00 | 0.65 | 1.73 | 31.13 | 356.00 | 350.00 | 6.00 | 37.13 |
| 49.00 | 50.00 | 12 | 30 | 120 | 11.00 | 5 | 55.00 | 3.00 | 2.74 | 690.00 | 0.98 | 6.78 | 29.40 | 356.00 | 351.00 | 5.00 | 34.40 |
| 50.00 | 53.00 | 2 | 32 | 120 | 11.00 | 6 | 66.00 | 3.00 | 3.29 | 63.00 | 1.38 | 0.87 | 22.62 | 356.00 | 355.00 | 1.00 | 23.62 |
| 51.00 | 52.00 | 9 | 9 | 120 | 11.00 | 3 | 33.00 | 2.00 | 3.57 | 326.00 | 2.52 | 8.21 | 30.48 | 356.00 | 349.00 | 7.00 | 37.48 |
| 52.00 | 53.00 | 2 | 11 | 120 | 11.00 | 4 | 44.00 | 3.00 | 2.19 | 80.00 | 0.65 | 0.52 | 22.27 | 356.00 | 350.00 | 6.00 | 28.27 |
| 53.00 | 57.00 | 4 | 47 | 120 | 11.00 | 6 | 66.00 | 3.00 | 3.29 | 242.00 | 1.38 | 3.33 | 21.75 | 356.00 | 350.00 | 6.00 | 27.75 |
| 54.00 | 55.00 | 3 | 3 | 120 | 11.00 | 2 | 22.00 | 2.00 | 2.38 | 82.00 | 1.19 | 0.97 | 25.28 | 356.00 | 350.00 | 6.00 | 31.28 |
| 55.00 | 56.00 | 6 | 9 | 120 | 11.00 | 3 | 33.00 | 2.00 | 3.57 | 169.00 | 2.52 | 4.26 | 24.31 | 356.00 | 350.00 | 6.00 | 30.31 |
| 56.00 | 57.00 | 7 | 16 | 120 | 11.00 | 4 | 44.00 | 3.00 | 2.19 | 251.00 | 0.65 | 1.63 | 20.05 | 356.00 | 349.00 | 7.00 | 27.05 |
| 57.00 | 62.00 | 2 | 65 | 120 | 11.00 | 7 | 77.00 | 4.00 | 2.32 | 257.00 | 0.54 | 1.39 | 18.42 | 356.00 | 348.00 | 8.00 | 26.42 |
| 58.00 | 59.00 | 3 | 3 | 120 | 11.00 | 2 | 22.00 | 2.00 | 2.38 | 107.00 | 1.19 | 1.27 | 27.89 | 356.00 | 351.00 | 5.00 | 32.89 |
| 59.00 | 60.00 | 6 | 9 | 120 | 11.00 | 3 | 33.00 | 2.00 | 3.57 | 242.00 | 2.52 | 6.10 | 26.62 | 356.00 | 350.00 | 6.00 | 32.62 |
| 60.00 | 61.00 | 9 | 18 | 120 | 11.00 | 4 | 44.00 | 3.00 | 2.19 | 339.00 | 0.65 | 2.20 | 20.52 | 356.00 | 349.00 | 7.00 | 27.52 |
| 61.00 | 62.00 | 5 | 23 | 120 | 11.00 | 5 | 55.00 | 3.00 | 2.74 | 131.00 | 0.98 | 1.29 | 18.32 | 356.00 | 348.00 | 8.00 | 26.32 |
| 62.00 | 63.00 | 2 | 90 | 120 | 11.00 | 8 | 88.00 | 4.00 | 2.65 | 147.00 | 0.69 | 1.02 | 17.03 | 356.00 | 347.00 | 9.00 | 26.03 |
| 63.00 | 64.00 | 7 | 97 | 120 | 11.00 | 8 | 88.00 | 4.00 | 2.65 | 311.00 | 0.69 | 2.15 | 16.01 | 356.00 | 347.00 | 9.00 | 25.01 |
| 64.00 | 65.00 | 4 | 280 | 120 | 11.00 | 14 | 154.00 | 6.00 | 2.14 | 319.00 | 0.30 | 0.95 | 13.86 | 355.00 | 350.00 | 5.00 | 18.86 |
| 65.00 | 75.00 | 2 | 362 | 1300 | 11.00 | 16 | 176.00 | 6.00 | 2.45 | 703.00 | 0.38 | 2.67 | 12.91 | 348.00 | 348.00 | 0.00 | 12.91 |
| 66.00 | 67.00 | 3 | 3 | 108 | 11.00 | 2 | 22.00 | 2.00 | 2.38 | 387.00 | 1.19 | 4.60 | 38.34 | 351.00 | 349.00 | 2.00 | 40.34 |
| 67.00 | 68.00 | 6 | 9 | 541 | 11.00 | 3 | 33.00 | 2.00 | 3.57 | 452.00 | 2.52 | 11.39 | 33.74 | 351.00 | 346.00 | 5.00 | 38.74 |
| 68.00 | 74.00 | 8 | 17 | 352 | 11.00 | 4 | 44.00 | 3.00 | 2.19 | 752.00 | 0.65 | 4.89 | 22.35 | 351.00 | 347.00 | 4.00 | 26.35 |
| 69.00 | 71.00 | 4 | 4 | 675 | 11.00 | 3 | 33.00 | 2.00 | 3.57 | 403.00 | 2.52 | 10.15 | 35.81 | 352.00 | 349.00 | 3.00 | 38.81 |
| 70.00 | 71.00 | 2 | 2 | 675 | 11.00 | 2 | 22.00 | 2.00 | 2.38 | 168.00 | 1.19 | 2.00 | 27.66 | 352.00 | 348.00 | 4.00 | 31.66 |


| $\begin{aligned} & \text { Zone } \\ & \text { Number } \end{aligned}$ | $\begin{array}{\|c} \hline \text { Connects } \\ \text { to Zone } \end{array}$ | Number <br> of Pumps <br> in Zone | Accum Pumps in Zone | Gals/day per Pump | Max Flow Per Pump (gpm) | $\begin{gathered} \text { Max } \\ \text { Sim Ops } \end{gathered}$ | Max Flow (GPM) | Pipe Size (inches) | Max <br> Velocity (FPS) | $\begin{gathered} \text { Length of Main } \\ \text { this Zone } \end{gathered}$ | Friction Loss <br> Factor <br> $(\mathrm{ft} / 100 \mathrm{ft})$ | Friction Loss This Zone | $\begin{array}{\|l} \text { Accum Fric } \\ \text { Loss (feet) } \end{array}$ | Max Main Elevation | Minimum Pump Elevation | Static Head (feet) | Total Dynamic Head (ft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| This spreadsheet was calculated using pipe diameters for: SDR11HDPE |  |  |  |  |  |  |  |  |  | Friction loss calculations were based on a Constant for inside roughness "C" of: 150 |  |  |  |  |  |  |  |
| 71.00 | 73.00 | 2 | 8 | 675 | 11.00 | 3 | 33.00 | 2.00 | 3.57 | 239.00 | 2.52 | 6.02 | 25.66 | 352.00 | 347.00 | 5.00 | 30.66 |
| 72.00 | 73.00 | 4 | 4 | 675 | 11.00 | 3 | 33.00 | 2.00 | 3.57 | 398.00 | 2.52 | 10.03 | 29.67 | 352.00 | 350.00 | 2.00 | 31.67 |
| 73.00 | 74.00 | 4 | 16 | 675 | 11.00 | 4 | 44.00 | 3.00 | 2.19 | 335.00 | 0.65 | 2.18 | 19.64 | 352.00 | 350.00 | 2.00 | 21.64 |
| 74.00 | 75.00 | 3 | 36 | 250 | 11.00 | 6 | 66.00 | 3.00 | 3.29 | 524.00 | 1.38 | 7.22 | 17.46 | 351.00 | 346.00 | 5.00 | 22.46 |
| 75.00 | 76.00 | 9 | 407 | 426 | 11.00 | 17 | 187.00 | 6.00 | 2.60 | 1,293.00 | 0.42 | 5.49 | 10.24 | 348.00 | 346.00 | 2.00 | 12.24 |
| 76.00 | 100.00 | 5 | 412 | 554 | 11.00 | 18 | 198.00 | 6.00 | 2.75 | 884.00 | 0.47 | 4.18 | 4.75 | 346.00 | 345.00 | 1.00 | 5.75 |
| 77.00 | 78.00 | 3 | 3 | 355 | 11.00 | 2 | 22.00 | 2.00 | 2.38 | 108.00 | 1.19 | 1.28 | 63.23 | 347.00 | 336.00 | 11.00 | 74.23 |
| 78.00 | 79.00 | 6 | 9 | 465 | 11.00 | 3 | 33.00 | 2.00 | 3.57 | 411.00 | 2.52 | 10.35 | 61.95 | 347.00 | 330.00 | 17.00 | 78.95 |
| 79.00 | 80.00 | 9 | 18 | 356 | 11.00 | 4 | 44.00 | 3.00 | 2.19 | 1,181.00 | 0.65 | 7.68 | 51.60 | 347.00 | 330.00 | 17.00 | 68.60 |
| 80.00 | 81.00 | 12 | 30 | 701 | 11.00 | 5 | 55.00 | 3.00 | 2.74 | 1,243.00 | 0.98 | 12.21 | 43.92 | 346.00 | 330.00 | 16.00 | 59.92 |
| 81.00 | 100.00 | 15 | 45 | 656 | 11.00 | 6 | 66.00 | 3.00 | 3.29 | 2,261.00 | 1.38 | 31.14 | 31.71 | 346.00 | 340.00 | 6.00 | 37.71 |
| 100.00 | 100.00 | 0 | 457 | 0 | 11.00 | 19 | 209.00 | 6.00 | 2.90 | 110.00 | 0.52 | 0.57 | 0.57 | 344.00 | 344.00 | 0.00 | 0.57 |
| 300.00 | 306.00 | 0 | 0 | 0 | 11.00 | 0 | 220.00 | 6.00 | 3.06 | 16,946.00 | 0.57 | 97.31 | 114.49 | 352.00 | 340.00 | 12.00 | 126.49 |
| On LS | S 300.00 |  | GPD | 100,0 | 000.000 | GPM: | 220 | 00 Ty | e: | C Des |  |  |  |  |  |  |  |
| 301.00 | 302.00 | 3 | 3 | 675 | 11.00 | 2 | 22.00 | 2.00 | 2.38 | 296.00 | 1.19 | 3.52 | 29.40 | 351.00 | 344.00 | 7.00 | 36.40 |
| 302.00 | 305.00 | 3 | 6 | 675 | 11.00 | 3 | 33.00 | 2.00 | 3.57 | 270.00 | 2.52 | 6.80 | 25.88 | 351.00 | 336.00 | 15.00 | 40.88 |
| 303.00 | 304.00 | 3 | 3 | 675 | 11.00 | 2 | 22.00 | 2.00 | 2.38 | 125.00 | 1.19 | 1.49 | 21.80 | 351.00 | 343.00 | 8.00 | 29.80 |
| 304.00 | 305.00 | 1 | 4 | 675 | 11.00 | 3 | 33.00 | 2.00 | 3.57 | 49.00 | 2.52 | 1.23 | 20.31 | 351.00 | 347.00 | 4.00 | 24.31 |
| 305.00 | 306.00 | 1 | 11 | 675 | 11.00 | 4 | 44.00 | 3.00 | 2.19 | 293.00 | 0.65 | 1.90 | 19.08 | 351.00 | 345.00 | 6.00 | 25.08 |
| 306.00 | 306.00 | 0 | 11 | 0 | 11.00 | 4 | 264.00 | 8.00 | 2.17 | 7,700.00 | 0.22 | 17.18 | 17.18 | 351.00 | 351.00 | 0.00 | 17.18 |



| Zone Number | Connects to Zone | Accumulated Total of Pumps this Zone | Pipe Size (inches) | Gallons per 100 lineal feet | Length of Zone | Capacity of Zone | Average Daily Flow | Average Fluid Changes per Day | Average Retention Time (Hr) | Accumulated Retention Time (Hr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| This spreadsheet was calculated using pipe diameters for: SDR11HDPE |  |  |  |  |  |  | Gals per Day per Dwelling 120 |  |  |  |
| 36.00 | 37.00 | 28 | 3.00 | 33.47 | 408.00 | 136.54 | 3,360 | 24.61 | 0.98 | 3.77 |
| 37.00 | 42.00 | 90 | 4.00 | 55.31 | 53.00 | 29.32 | 10,800 | 368.40 | 0.07 | 2.80 |
| 38.00 | 39.00 | 9 | 2.00 | 15.40 | 242.00 | 37.27 | 1,080 | 28.97 | 0.83 | 6.54 |
| 39.00 | 40.00 | 18 | 3.00 | 33.47 | 301.00 | 100.73 | 2,160 | 21.44 | 1.12 | 5.72 |
| 40.00 | 41.00 | 30 | 3.00 | 33.47 | 430.00 | 143.91 | 3,600 | 25.02 | 0.96 | 4.60 |
| 41.00 | 42.00 | 44 | 3.00 | 33.47 | 595.00 | 199.13 | 5,280 | 26.52 | 0.91 | 3.64 |
| 42.00 | 43.00 | 134 | 4.00 | 55.31 | 100.00 | 55.31 | 16,080 | 290.71 | 0.08 | 2.73 |
| 43.00 | 44.00 | 164 | 4.00 | 55.31 | 243.00 | 134.41 | 19,680 | 146.42 | 0.16 | 2.65 |
| 44.00 | 64.00 | 175 | 4.00 | 55.31 | 1,305.00 | 721.84 | 21,000 | 29.09 | 0.82 | 2.49 |
| 45.00 | 64.00 | 4 | 2.00 | 15.40 | 112.00 | 17.25 | 480 | 27.82 | 0.86 | 2.52 |
| 46.00 | 47.00 | 3 | 2.00 | 15.40 | 102.00 | 15.71 | 360 | 22.91 | 1.05 | 8.16 |
| 47.00 | 48.00 | 9 | 2.00 | 15.40 | 431.00 | 66.39 | 1,080 | 16.27 | 1.48 | 7.11 |
| 48.00 | 49.00 | 18 | 3.00 | 33.47 | 266.00 | 89.02 | 2,160 | 24.26 | 0.99 | 5.64 |
| 49.00 | 50.00 | 30 | 3.00 | 33.47 | 690.00 | 230.92 | 3,600 | 15.59 | 1.54 | 4.65 |
| 50.00 | 53.00 | 32 | 3.00 | 33.47 | 63.00 | 21.08 | 3,840 | 182.13 | 0.13 | 3.11 |
| 51.00 | 52.00 | 9 | 2.00 | 15.40 | 326.00 | 50.21 | 1,080 | 21.51 | 1.12 | 4.58 |
| 52.00 | 53.00 | 11 | 3.00 | 33.47 | 80.00 | 26.77 | 1,320 | 49.30 | 0.49 | 3.46 |
| 53.00 | 57.00 | 47 | 3.00 | 33.47 | 242.00 | 80.99 | 5,640 | 69.64 | 0.34 | 2.98 |
| 54.00 | 55.00 | 3 | 2.00 | 15.40 | 82.00 | 12.63 | 360 | 28.50 | 0.84 | 5.10 |
| 55.00 | 56.00 | 9 | 2.00 | 15.40 | 169.00 | 26.03 | 1,080 | 41.49 | 0.58 | 4.26 |
| 56.00 | 57.00 | 16 | 3.00 | 33.47 | 251.00 | 84.00 | 1,920 | 22.86 | 1.05 | 3.68 |
| 57.00 | 62.00 | 65 | 4.00 | 55.31 | 257.00 | 142.15 | 7,800 | 54.87 | 0.44 | 2.63 |
| 58.00 | 59.00 | 3 | 2.00 | 15.40 | 107.00 | 16.48 | 360 | 21.84 | 1.10 | 5.76 |
| 59.00 | 60.00 | 9 | 2.00 | 15.40 | 242.00 | 37.27 | 1,080 | 28.97 | 0.83 | 4.67 |
| 60.00 | 61.00 | 18 | 3.00 | 33.47 | 339.00 | 113.45 | 2,160 | 19.04 | 1.26 | 3.84 |
| 61.00 | 62.00 | 23 | 3.00 | 33.47 | 131.00 | 43.84 | 2,760 | 62.95 | 0.38 | 2.58 |
| 62.00 | 63.00 | 90 | 4.00 | 55.31 | 147.00 | 81.31 | 10,800 | 132.82 | 0.18 | 2.20 |
| 63.00 | 64.00 | 97 | 4.00 | 55.31 | 311.00 | 172.02 | 11,640 | 67.67 | 0.35 | 2.01 |
| 64.00 | 65.00 | 280 | 6.00 | 119.90 | 319.00 | 382.48 | 33,600 | 87.85 | 0.27 | 1.66 |
| 65.00 | 75.00 | 362 | 6.00 | 119.90 | 703.00 | 842.89 | 45,800 | 54.34 | 0.44 | 1.39 |
| 66.00 | 67.00 | 3 | 2.00 | 15.40 | 387.00 | 59.61 | 324 | 5.44 | 4.42 | 7.01 |
| 67.00 | 68.00 | 9 | 2.00 | 15.40 | 452.00 | 69.62 | 3,570 | 51.28 | 0.47 | 2.59 |
| 68.00 | 74.00 | 17 | 3.00 | 33.47 | 752.00 | 251.67 | 6,386 | 25.37 | 0.95 | 2.13 |
| 69.00 | 71.00 | 4 | 2.00 | 15.40 | 403.00 | 62.07 | 2,700 | 43.50 | 0.55 | 2.14 |
| 70.00 | 71.00 | 2 | 2.00 | 15.40 | 168.00 | 25.88 | 1,350 | 52.17 | 0.46 | 2.05 |

## BLUEBIRD <br> TERRACE

Attachment A
Figure
Showing the E-One
Analysis Area
Not to Scale

## ATTACHMENT

B

PUMP PERFORMANCE CURVE

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## ElONE SPD PUMP PERFORMANCE CURVE



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## ATTACHMENT

C

## HYDRAULIC GRADE LINE

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## NOTES:

1. THIS PAGE'S PROFILE EXISTING GROUND DATA WAS SCALED FROM "MOREAU INDUSTRIA PARK" BY STEARNS \& WHELER; RECORD DRAWINGS STAMPED 1/31/96 BY HOWARD AENSON LIFEVER NYS PE

| TOWN OF MOREAU <br> SARATOGA COUNTY * NEW YORK <br> SEWER DISTRICT NO. 1 EXTENSION 5 <br> YDRAULIC GRADE LINE |  |  |
| :---: | :---: | :---: |
| DESIGNED BY JAK dRAWN BY $\qquad$ REVEWED BY $\qquad$ |  | $\begin{array}{lr} \text { DATE } & 09 / 24 / 20 \\ \text { SCALE } & \text { AS NOTED } \\ \text { SHEET } & 3 \\ \hline \end{array}$ |

## ATTACHMENT

D

## LIFT STATION DESIGN BASIS PUMP

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## NP 3171 SH 3~ 275

Patented self cleaning semi-open channel impeller, ideal for pumping in waste water applications. Possible to be upgraded with Guide-pin ${ }^{\circledR}$ for even better clogging resistance. Modular based design with high adaptation grade.

## Technical specification



Curves according to: Water, pure , $39.2^{\circ} \mathrm{F}, 62.42 \mathrm{lb} / \mathrm{ft}^{3}, 1.6891 \mathrm{E}-5 \mathrm{ft}^{2} / \mathrm{s}$


Configuration

| Motor number | Installation type |
| :--- | :--- |
| N3171.095 25-18-2AA-W | P-Semi permanent, Wet |
| 35hp |  |
| Impeller diameter | Discharge diameter |
| 195 mm | $315 / 16$ inch |

195 mm

## Materials

Impeller
Impeller diameter
Hard-Iron ${ }^{\text {M }}$

Discharge diameter
3 15/16 inch

Inlet diameter
150 mm
Maximum operating speed
3530 rpm

## Number of blades

2

## Max. fluid temperature

$40^{\circ} \mathrm{C}$

| Project | Created by | Ian Belczyk |
| :--- | :--- | :--- |
| Block | Created on | $11 / 6 / 2020$ |

NP 3171 SH 3~ 275
Technical specification


Motor - General

| Motor number | Phases | Rated speed | Rated power |
| :---: | :---: | :---: | :---: |
|  | 3~ | 3530 rpm | 35 hp |
| ATEX approved | Number of poles | Rated current | Stator variant |
| FM | 2 | 40 A | 9 |
| Frequency | Rated voltage | Insulation class | Type of Duty |
| 60 Hz | 460 V | H | S1 |
| Version code |  |  |  |
| 095 |  |  |  |
| Motor - Technical |  |  |  |
| Power factor - 1/1 Load | Motor efficiency-1/1 Load | Total moment of inertia | Starts per hour max. |
| 0.91 | 91.0\% | $1.77 \mathrm{lb} \mathrm{ft}^{2}$ | 30 |
| Power factor - 3/4 Load | Motor efficiency-3/4 Load | Starting current, direct starting |  |
| 0.89 | 91.5 \% | 292 A |  |
| Power factor-1/2 Load | Motor efficiency-1/2 Load | Starting current, star-delta |  |
| 0.82 | 92.0\% | 97.3 A |  |


| Project | Created by | lan Belczyk |
| :--- | :--- | :--- |
| Block | Created on | $11 / 6 / 2020$ |

## NP 3171 SH 3~ 275

## Performance curve

## Duty point

a xylem brand
Flow
Head
629 US g.p.m.
129 ft


## NP 3171 SH 3~ 275

Duty Analysis


Curves according to: Water, pure , $39.2^{\circ} \mathrm{F}, 62.42 \mathrm{lb} / \mathrm{ft}^{3}, 1.6891 \mathrm{E}-5 \mathrm{ft}^{2} / \mathrm{s}$


Operating characteristics

| Pumps / <br> Systems | Flow | Head | Shaft power | Flow | Head | Shaft power | Hydr.eff. | Specific <br> Energy |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 629 US g.p.m. | 129 ft | 33.2 hp | 629 | US g.p.m. | 129 ft | 33.2 hp | $61.8 \%$ | $721 \mathrm{kWh} / \mathrm{US} \mathrm{M( }$ |


| Project | Created by | lan Belczyk | Last update |
| :--- | :--- | :--- | :--- |
| Block | Created on | $11 / 6 / 2020$ | 11/6/2020 |

NP 3171 SH 3~ 275
VFD Curve

Curves according to: Water, pure, $39.2^{\circ} \mathrm{F}, 62.42 \mathrm{lb} / \mathrm{ft}^{3}, 1.6891 \mathrm{E}-5 \mathrm{ft}^{2} / \mathrm{s}$


NP 3171 SH 3~ 275
VFD Analysis


Operating characteristics

| Pumps / Systems | Frequency | Flow | Head | Shaft power | Flow | Head | Shaft power | Hydr.eff. | Specific Energy | NPSHre |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 60 Hz | 629 US g.p.m. | 129 ft | 33.2 hp | 629 US g.p.m. | 129 ft | 33.2 hp | 61.8 \% | 721 kWh/US M | 28 ft |
| 1 | 55 Hz | 540 US g.p.m. | 116 ft | 25.3 hp | 540 US g.p.m. | 116 ft | 25.3 hp | 62.6\% | 631 kWh/US M | 21.7 ft |
| 1 | 50 Hz | 448 US g.p.m. | 104 ft | 18.8 hp | 448 US g.p.m. | 104 ft | 18.8 hp | 62.8\% | $566 \mathrm{kWh} / \mathrm{US} \mathrm{M}$ | 16 ft |
| 1 | 45 Hz | 345 US g.p.m. | 93.4 ft | 13.3 hp | 345 US g.p.m. | 93.4 ft | 13.3 hp | 61.2 \% | 526 kWh/US M | 11.1 ft |
| 1 | 40 Hz | 223 US g.p.m. | 84.4 ft | 8.73 hp | 223 US g.p.m. | 84.4 ft | 8.73 hp | 54.6 \% | 545 kWh/US M | 7.41 ft |


| Project | Created by | lan Belczyk | Last update |
| :--- | :--- | :--- | :--- |
| Block | Created on | $11 / 6 / 2020$ |  |



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| Pump type: <br> Application: | Submersible sewage Pump Waste water |
| :---: | :---: |
| Pump data |  |
| Solids passage | 4" |
| Discharge/ Suction diameter | r 4"/ 5" |
| Impeller type: | Vortex |
| Impeller diameter | 315-235 |
| Recommended min. flow | 95 USGPM |
| Weight | 661 lbs |
| Motor |  |
| Mains: | $60 \mathrm{c} / \mathrm{s}-3$ phase |
| Rated horse power | 52.4 HP |
| Rated electrical power | 45.3 kW |
| Rated kVA | 52.9 kVA |
| Nominal speed | 1730 rpm SYSTEM CURVE |
| Motor efficiency | 86 \% |
| Power factor (cos phi) | 0.86 |
| Degree of protection | IP 68 |
| Isolation class | $\mathrm{F}\left(311^{\circ} \mathrm{F}\right)$ |
| Max. water temperature | $104{ }^{\circ} \mathrm{F}$ |
| Standard cable length | 33 ft |
| Materials |  |
| Pump casing | Cast iron (ASTM A-48 class 35) <br> S.g cast iron (ASTM A-445 Gr.60-46-18) |
| Impeller |  |
| Motor unit | Cast iron (ASTM A-48 class 35) |
| Shaft | AISI 431 |
| Bolts | AISI 316 |
| Elastomers | Nitrile (NBR) or neoprene (CR) |
|  | Alt: viton (FPM) |
| Electrical cable | Neoprene (CR) |
| Seal lubrication | Oil |
| Seal pump side | Silicon carbide - silicon carbide |
| Seal motor side | Carbon - Ceramic |
| Coating | Two components polyurethane |

## Installation options

Guide bar coupling

Freestanding
Including support

Dry Installation
Including cooling system

OWK 100 or OWK 150

4" hose connection or 4" NPT connection
vertical or horizontal discharge 4" suction 5 "

## Options available

- Version with cooling system
- Cable protective sheathing (AISI 316)
- Water detector in motor and oil chamber




## Connections



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## ATTACHMENT <br> E

## BUOYANCY CALCULATIONS

WET WELL \& VALVE VAULT

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$\qquad$
$\qquad$ OF 2

CHECKED BY $\qquad$
$\qquad$
CLIENT \& PROJ. NAME MORERG, NY - DISTRICT $/$ EXT. \#S
PROJ. NO. $201010^{7}$

Buoybncy Calculatom - Wet Well


Werent of Compoments
(A) Top sine

$$
\begin{array}{lr}
\pi f^{2} h=\pi(5.67 F T)^{2}(0.67 F r)= & 67.63 F^{2} \\
-H A T C H=-(4.0 F T)(6.0 G T)(0.67 F T)= & -16.08 F T^{2}
\end{array}
$$

(B) walls

$$
\pi h\left(r_{0}^{2}-r_{1}^{2}\right)=\pi(15 \mathrm{f})\left[(5.6 T \mathrm{f})^{2}-(5.0 \mathrm{fT})^{2}\right]=336.7 \mathrm{f}
$$

(C)

$$
\pi r^{2} h=\pi(6.17 \mathrm{fr})^{2}(0.67 \mathrm{~m})=
$$

$$
80.1 \mathrm{fr}^{3}
$$

(D)

$$
\begin{aligned}
& A_{2}=\pi r^{2}= \pi\left(6.17 \pi+\left(\frac{1516}{2}\right)\right)^{2}=591.1 \mathrm{Fr}^{2} \\
& 13.726 T
\end{aligned}
$$

OLsRosement Vocurte

$$
\begin{aligned}
& \text { Solls (FRUETRUN CQU.) } \\
& \alpha=30^{\circ} \\
& A_{1}=\pi r^{2}=\pi(6.17 \mathrm{fr})^{2}=119.5 \mathrm{cr}^{2}
\end{aligned}
$$

$$
\forall=\frac{1}{3} h\left(A_{1}+\sqrt{A_{1} A_{2}}+A_{2}\right)-A_{3}
$$

$$
\forall=\pi r^{2} h=\pi(5.67 \sigma T)^{2}(344.5 \mathrm{fr}-329.4 \mathrm{fr})
$$

$$
=1524.3 \mathrm{FT}^{3}(\text { анин })
$$

$$
=\frac{1}{3}(15.15 r)\left(119.55^{2}+\sqrt{119.5+591.16 r^{2}+581.16 r^{2}}\right)
$$

$$
-\pi(5.57 \sigma \pi)^{2}(15.15 r)
$$

$$
+\pi r^{2} h=\pi(6.17 f r)^{2}(0.67 \mathrm{Fr})=80.1 f r^{3}(f \text { coNn })
$$

$$
=1524.3 \mathrm{fr}^{3}+80.1 \mathrm{fr}^{3}=1604.4 \mathrm{fr}^{3} .
$$

COMP. BY $\qquad$
CHECKED BY $\qquad$
$\qquad$
$\qquad$
PROJ. NO. 2018107
$\qquad$

Buovancy Calculation - Valve Vant
 Weloht of Compowerts
(1)

$$
\begin{aligned}
& \text { TOP SLAB } \\
& \left.(9.0 \mathrm{FT})(13.0 \mathrm{FT})(0.67 \mathrm{FT})=78.39 \mathrm{FT}^{3}=14 \mathrm{THT}\right)=-4.19 \mathrm{FT}^{3}
\end{aligned}
$$

(B) walls

$$
\begin{aligned}
& {[(2)(12.5 \mathrm{FT})+(2)(8.5 \mathrm{Ft})](8 \mathrm{FT})(0.5 \mathrm{FT}) } \\
&= 168.00 \mathrm{fT}^{3}
\end{aligned}
$$

(c) FLOOR

$$
(14.0 \mathrm{fT})(10.0 \mathrm{fT})(0.67 \mathrm{fT})=93.80 \mathrm{fT}
$$

(0)

Summbey

$$
\begin{gathered}
\overrightarrow{\left.F_{c}+F_{S}\right)} \frac{(50.4 \mathrm{kIP}+140 \mathrm{k} 1 \mathrm{P})}{65.5 \mathrm{k} 1 P}=2.9 \\
F_{O S}=2.9
\end{gathered}
$$

$$
\begin{aligned}
& \int F_{*}=\left(1049.69 \mathrm{FT}^{2}\right)(62.4 \% / \mathrm{FT})=65,50016 . \\
& F_{C}=(A)+(C)\left(150 \mathrm{k} / \mathrm{F}^{3}\right. \\
& =\left(33600 \mathrm{fr}^{3}\right)\left(150 \mathrm{~m} / \mathrm{Fr}^{3}\right)=50,400 / \mathrm{b} \\
& =\left(1169 \mathrm{er}^{3}\right)\left(120 \mathrm{lb} / \mathrm{m}^{3}\right)=140,300 \mathrm{lb}
\end{aligned}
$$

$$
\begin{aligned}
& \text { soll (Frustrum equ.) } \\
& A_{1}=(14.0 \mathrm{Fr})(100 \mathrm{Fr})=140 \mathrm{Fr}^{2} \\
& A_{2}[(14.05 T+8.176 T) \times \\
& [10.0 \mathrm{fr}+8.17 \mathrm{Ft})]=402.86 \mathrm{ch}^{3} \\
& \forall_{s}=\frac{1}{3} h\left(A_{1}+\sqrt{A_{1} A_{2}}+A_{2}\right) \\
& =\frac{1}{3}(8.17 \pi)\left(140 r^{\frac{7}{7}}+\sqrt{\left(40.402 .87^{7}\right.}+402.8 \mathrm{~F}_{7}^{2}\right) \\
& =21256 r^{3}-(13 R)(q / T)(8.17 \mathrm{FT}) \\
& =7169.1 \mathrm{Cr}^{3} 955
\end{aligned}
$$

## ATTACHMENT

F

## SYSTEM SCHEMATIC

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- PROPOSED FORCE MAIN
-     -         - EXISTING FORCE MAIN



## ATTACHMENT

## G

## SEWER MASTER METER READINGS

MARCH 2020 - DECEMBER 2020

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TOWN OF MOREAU

| VAN BUREN - SEWER - MASTER METER READINGS |  |  |  |  | BEG. 3/2/2020 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Date | Start Meter Reading | End Meter Reading | Gallons Pumped Per Day | Running Totals | Monthly Totals |
| 3/2/2020 | 0 | 70,000 | 70,000 | 70,000 |  |
| 3/3/2020 | 70000 | 143,850 | 73,850 | 143,850 |  |
| 3/4/2020 | 143850 | 213,181 | 69,331 | 213,181 |  |
| 3/5/2020 | 213181 | 291,035 | 77,854 | 291,035 |  |
| 3/6/2020 | 291035 | 359,150 | 68,115 | 359,150 |  |
| 3/7/2020 | 359150 | 427,900 | 68,750 | 427,900 |  |
| 3/8/2020 | 427900 | 515,600 | 87,700 | 515,600 |  |
| 3/9/2020 | 515600 | 600,800 | 85,200 | 600,800 |  |
| 3/10/2020 | 600800 | 685,949 | 85,149 | 685,949 |  |
| 3/11/2020 | 685949 | 754,135 | 68,186 | 754,135 |  |
| 3/12/2020 | 754135 | 839,140 | 85,005 | 839,140 |  |
| 3/13/2020 | 839140 | 909,000 | 69,860 | 909,000 |  |
| 3/14/2020 | 909000 | 972,537 | 63,537 | 972,537 |  |
| 3/15/2020 | 972537 | 1,056,100 | 83,563 | 1,056,100 |  |
| 3/16/2020 | 1056100 | 1,123,296 | 67,196 | 1,123,296 |  |
| 3/17/2020 | 1123296 | 1,183,200 | 59,904 | 1,183,200 |  |
| 3/18/2020 | 1183200 | 1,258,900 | 75,700 | 1,258,900 |  |
| 3/19/2020 | 1258900 | 1,343,722 | 84,822 | 1,343,722 |  |
| 3/20/2020 | 1343722 | 1,427,350 | 83,628 | 1,427,350 |  |
| 3/21/2020 | 1427350 | 1,500,000 | 72,650 | 1,500,000 |  |
| 3/22/2020 | 1500000 | 1,582,500 | 82,500 | 1,582,500 |  |
| 3/23/2020 | 1582500 | 1,678,370 | 95,870 | 1,678,370 |  |
| 3/24/2020 | 1678370 | 1,752,540 | 74,170 | 1,752,540 |  |
| 3/25/2020 | 1752540 | 1,824,550 | 72,010 | 1,824,550 |  |
| 3/26/2020 | 1824550 | 1,914,830 | 90,280 | 1,914,830 |  |
| 3/27/2020 | 1914830 | 1,984,870 | 70,040 | 1,984,870 |  |
| 3/28/2020 | 1984870 | 2,050,900 | 66,030 | 2,050,900 |  |
| 3/29/2020 | 2050900 | 2,125,250 | 74,350 | 2,125,250 |  |
| 3/30/2020 | 2125250 | 2,210,140 | 84,890 | 2,210,140 |  |
| 3/31/2020 | 2210140 | 2,278,580 | 68,440 | 2,278,580 | 2,278,580 |


| VAN BUREN - SEWER - MASTER METER READINGS |  |  |  |  | BEG. 3/2/2020 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 4/1/2020 | 2278580 | 2,348,660 | 70,080 |  |  |
| 4/2/2020 | 2348660 | 2,428,640 | 79,980 |  |  |
| 4/3/2020 | 2428640 | 2,505,690 | 77,050 |  |  |
| 4/4/2020 | 2505690 | 2,582,390 | 76,700 |  |  |
| 4/5/2020 | 2582390 | 2,649,520 | 67,130 |  |  |
| 4/6/2020 | 2649520 | 2,722,560 | 73,040 |  |  |
| 4/7/2020 | 2722560 | 2,795,620 | 73,060 |  |  |
| 4/8/2020 | 2795620 | 2,874,830 | 79,210 |  |  |
| 4/9/2020 | 2874830 | 2,957,700 | 82,870 |  |  |
| 4/10/2020 | 2957700 | 3,021,450 | 63,750 |  |  |
| 4/11/2020 | 3021450 | $3,085,420$ | 63,970 |  |  |
| 4/12/2020 | 3085420 | $3,160,150$ | 74,730 |  |  |
| 4/13/2020 | 3160150 | 3,247,520 | 87,370 |  |  |
| 4/14/2020 | 3247520 | $3,320,150$ | 72,630 |  |  |
| 4/15/2020 | 3320150 | $3,402,420$ | 82,270 |  |  |
| 4/16/2020 | 3402420 | $3,465,020$ | 62,600 |  |  |
| 4/17/2020 | 3465020 | 3,536,590 | 71,570 |  |  |
| 4/18/2020 | 3536590 | 3,601,890 | 65,300 |  |  |
| 4/19/2020 | 3601890 | 3,659,370 | 57,480 |  |  |
| 4/20/2020 | 3659370 | 3,729,060 | 69,690 |  |  |
| 4/21/2020 | 3729060 | 3,798,560 | 69,500 |  |  |
| 4/22/2020 | 3798560 | $3,874,520$ | 75,960 |  |  |
| 4/23/2020 | 3874520 | 3,947,510 | 72,990 |  |  |
| 4/24/2020 | 3947510 | 4,012,410 | 64,900 |  |  |
| 4/25/2020 | 4012410 | 4,097,450 | 85,040 |  |  |
| 4/26/2020 | 4097450 | 4,177,410 | 79,960 |  |  |
| 4/27/2020 | 4177410 | 4,245,500 | 68,090 |  |  |
| 4/28/2020 | 4245500 | 4,316,940 | 71,440 |  |  |
| 4/29/2020 | 4316940 | 4,391,020 | 74,080 |  |  |
| 4/30/2020 | 4391020 | 4,465,590 | 74,570 |  | 2,187,010 |



| VAN BUREN - SEWER - MASTER METER READINGS |  |  |  |  | BEG. 3/2/2020 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6/10/2020 | 7503550 | 7,589,35 | 85,800 |  |  |
| 6/11/2020 | 7589350 | 7,667,96 | 78,610 |  |  |
| 6/12/2020 | 7667960 | 7,743,930 | 75,970 |  |  |
| 6/13/2020 | 7743930 | 7,809,240 | 65,310 |  |  |
| 6/14/2020 | 7809240 | 7,867,710 | 58,470 |  |  |
| 6/15/2020 | 7867710 | 7,946,490 | 78,780 |  |  |
| 6/16/2020 | 7946490 | 8,027,130 | 80,640 |  |  |
| 6/17/2020 | 8027130 | 8,103,270 | 76,140 |  |  |
| 6/18/2020 | 8103270 | 8,184,440 | 81,170 |  |  |
| 6/19/2020 | 8184440 | 8,255,660 | 71,220 |  |  |
| 6/20/2020 | 8255660 | 8,317,180 | 61,520 |  |  |
| 6/21/2020 | 8317180 | 8,399,960 | 82,780 |  |  |
| 6/22/2020 | 8399960 | 8,468,660 | 68,700 |  |  |
| 6/23/2020 | 8468660 | 8,557,600 | 88,940 |  |  |
| 6/24/2020 | 8557600 | 8,651,350 | 93,750 |  |  |
| 6/25/2020 | 8651350 | 8,725,770 | 74,420 |  |  |
| 6/26/2020 | 8725770 | 8,797,020 | 71,250 |  |  |
| 6/27/2020 | 8797020 | 8,873,490 | 76,470 |  |  |
| 6/28/2020 | 8873490 | 8,962,070 | 88,580 |  |  |
| 6/29/2020 | 8962070 | 9,027,100 | 65,030 |  |  |
| 6/30/2020 | 9027100 | 9,104,510 | 77,410 |  | $(2,367,190)$ |
| 7/1/2020 | 9104510 | 9,174,010 | 69,500 |  |  |
| 7/2/2020 | 9174010 | 9,247,790 | 73,780 |  |  |
| 7/3/2020 | 9247790 | 9,321,770 | 73,980 |  |  |
| 7/4/2020 | 9321770 | 9,395,550 | 73,780 |  |  |
| 7/5/2020 | 9395550 | 9,477,500 | 81,950 |  |  |
| 7/6/2020 | 9477500 | 9,557,900 | 80,400 |  |  |
| 7/7/2020 | 9557900 | 9,637,560 | 79,660 |  |  |
| 7/8/2020 | 9637560 | 9,709,200 | 71,640 |  |  |
| 7/9/2020 | 9709200 | 9,791,790 | 82,590 |  |  |
| 7/10/2020 | 9791790 | 9,873,240 | 81,450 |  |  |
| 7/11/2020 | 9873240 | 9,948,590 | 75,350 |  |  |
| 7/12/2020 | 9948590 | 10,022,490 | 73,900 |  |  |
| 7/13/2020 | 10022490 | 10,101,500 | 79,010 |  |  |
| 7/14/2020 | 10101500 | 10,178,000 | 76,500 |  |  |
| 7/15/2020 | 10178000 | 10,239,300 | 61,300 |  |  |
| 7/16/2020 | 10239300 | 10,320,800 | 81,500 |  |  |
| 7/17/2020 | 10320800 | 10,384,230 | 63,430 |  |  |
| 7/18/2020 | 10384230 | 10,466,400 | 82,170 |  |  |
| 7/19/2020 | 10466400 | 10,551,100 | 84,700 |  |  |

TOWN OF MOREAU



TOWN OF MOREAU


| VAN BUREN - SEWER - MASTER METER READINGS |  |  |  | BEG. 3/2/2020 |
| :---: | :---: | :---: | :---: | :---: |
| 11/17/2020 | 19770670 | 19,849,670 | 79,000 |  |
| 11/18/2020 | 19849670 | 19,922,470 | 72,800 |  |
| 11/19/2020 | 19922470 | 19,987,510 | 65,040 |  |
| 11/20/2020 | 19987510 | 20,056,840 | 69,330 |  |
| 11/21/2020 | 20056840 | 20,126,180 | 69,340 |  |
| 11/22/2020 | 20126180 | 20,203,740 | 77,560 |  |
| 11/23/2020 | 20203740 | 20,287,640 | 83,900 |  |
| 11/24/2020 | 20287640 | 20,367,080 | 79,440 |  |
| 11/25/2020 | 20367080 | 20,447,060 | 79,980 |  |
| 11/26/2020 | 20447060 | 20,525,600 | 78,540 |  |
| 11/27/2020 | 20525600 | 20,571,460 | 45,860 |  |
| 11/28/2020 | 20571460 | 20,655,750 | 84,290 |  |
| 11/29/2020 | 20655750 | 20,740,260 | 84,510 |  |
| 11/30/2020 | 20740260 | 20,824,900 | 84,640 | 2,320,180 |
| 12/1/2020 | 20824900 | 20,890,500 | 65,600 |  |
| 12/2/2020 | 20890500 | 20,977,210 | 86,710 |  |
| 12/3/2020 | 20977210 | 21,051,750 | 74,540 |  |
| 12/4/2020 | 21051750 | 21,134,320 | 82,570 |  |
| 12/5/2020 | 21134320 | 21,210,010 | 75,690 |  |
| 12/6/2020 | 21210010 | 21,281,080 | 71,070 |  |
| 12/7/2020 | 21281080 | 21,357,480 | 76,400 |  |
| 12/8/2020 | 21357480 | 21,440,000 | 82,520 |  |
| 12/9/2020 | 21440000 | 21,512,330 | 72,330 |  |
| 12/10/2020 | 21512330 | 21,593,580 | 81,250 |  |
| 12/11/2020 | 21593580 | 21,663,080 | 69,500 |  |
| 12/12/2020 | 21663080 | 21,738,090 | 75,010 |  |
| 12/13/2020 | 21738090 | 21,834,950 | 96,860 |  |
| 12/14/2020 | 21834950 | 21,916,100 | 81,150 |  |
| 12/15/2020 | 21916100 | 21,996,030 | 79,930 |  |
| 12/16/2020 | 21996030 | 22,079,550 | 83,520 |  |
| 12/17/2020 | 22079550 | 22,141,950 | 62,400 |  |
| 12/18/2020 | 22141950 | 22,203,980 | 62,030 |  |
| 12/19/2020 | 22203980 | 22,287,550 | 83,570 |  |
| 12/20/2020 | 22287550 | 22,367,950 | 80,400 |  |
| 12/21/2020 | 22367950 | 22,448,540 | 80,590 |  |
| 12/22/2020 | 22448540 | 22,522,850 | 74,310 |  |
| 12/23/2020 | 22522850 | 22,591,410 | 68,560 |  |
| 12/24/2020 | 22591410 | 22,674,950 | 83,540 |  |
| 12/25/2020 | 22674950 | 22,746,450 | 71,500 |  |
| 12/26/2020 | 22746450 | 22,816,660 | 70,210 |  |


| VAN BUREN - SEWER - MASTER METER READINGS |  |  |  | BEG. 3/2/2020 |
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| 12/27/2020 | 22816660 | 22,902,450 | 85,790 |  |
| 12/28/2020 | 22902450 | 22,996,650 | 94,200 |  |
| 12/29/2020 | 22996650 | 23,071,140 | 74,490 |  |
| 12/30/2020 | 23071140 | 23,159,330 | 88,190 |  |
| 12/31/2020 | 23159330 | 23,235,022 | 75,692 | 2410122 |
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## APPENDIXC CITY OF GLENS FALLS LETTER

Water \& Sewer Department Telephone: [518] 761-3850 24 Hr. Water \& Sewer Emergencies: [518] 761-3857

- Fax: [518] 761-3862
- www.ciryofglensfalls.com

Raymond Apy
Feb. 18, 2022
Chief Executive Officer
Northeastern Biochar Solutions
Mr. Apy
Per our discussion on December 14, 2021, the City of Glens Falls Wastewater Treatment Plant can receive the profile and volume of wastewater as stated in said meeting.

At this time your facility would not be considered a categorical industrial user but as with all industrial customers that send wastewater to the City of Glens Falls Wastewater Treatment Plant, you will be required to meet the Glens Falls City Code 177 Article VII, Discharge Requirements. Pretreatment will not be necessary unless the profile of your wastewater does not meet the Glens Falls Local Limits or causes pass through or interference with the wastewater treatment plant process.

I would like to reiterate that based on the data we have; the Town of Moreau is presently discharging around $75,000 \mathrm{gpd}$ to the City of Glens Falls WWTP and the Town of Moreau's purchased capacity is 190,000 gps. However, I do not know how that capacity is allocated among Moreau's 5 sewer district extensions. That is a question that you would have to ask the folks in Moreau as it is the responsibility of the Town of Moreau to appoint capacity in each of their sewer districts.

If you have any questions or need clarification, please contact me.
Thank you,


Christopher S. Miller
Chief Operator
City of Glens Falls Wastewater Treatment Plant
2 Shermantown Rd.
Glens Falls, NY 12801
Phone: 518 761-3850 ext 119
Fax: 518761-3862
cmiller@cityofglensfalls.com

